

Suggestions for the Development of Design Criteria for Precision Deployment Mechanisms

**Presented at the Microdynamics Workshop,
Jet Propulsion Laboratory
June 24, 1999**

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The Prevailing Responsibilities of the Microdynamics Community

1. To clearly define what (if any) “modes” of microdynamic response constitute “failure” modes of the structure.

- What are the critical loads (i.e., disturbances) that the structure must sustain?
- What are the critical response modes (OR amplitudes) that must NOT be excited within the structure?

2. To clearly define design/validation guidelines and criteria which preclude microdynamic failure.

- We can’t “analyze” the “art” out of design, but we can identify deterministic relationships that facilitate the heuristic design process.
- We should be able to establish REASONABLE and ADEQUATE criteria. (e.g., Microdynamic equivalents to “knock-down” factors commonly used in stability of imperfect members?)

(Subject of this presentation)

Developing Design Guidelines and Criteria for Precision Deployment Mechanisms

- **Motivation:**

- Pressure to reduce the cost of space vehicles has spawned new sub-disciplines of design like precision deployable structures.
- Adequacy of any engineering design can only be defined relative to some accepted standards or criteria.
- No such criteria currently exist for the design of precision deployment mechanisms.

- **Precedent:**

- In the early 1960's, pressure to expand the capability of space vehicles simulated development of new sub-disciplines of design.
- Uniform design criteria were developed jointly by NASA, industry, and academia and were published in 15 Design Criteria Monographs.
- Since these fields were advancing substantially at the time, the monographs were “living documents” that have evolved over time

The “Anatomy” of the NASA Design Criteria SP’s from the 1960’s

The Background and Motivation: Filled gaps of knowledge and a need for uniformity AND conformity in the design of flight vehicle systems.

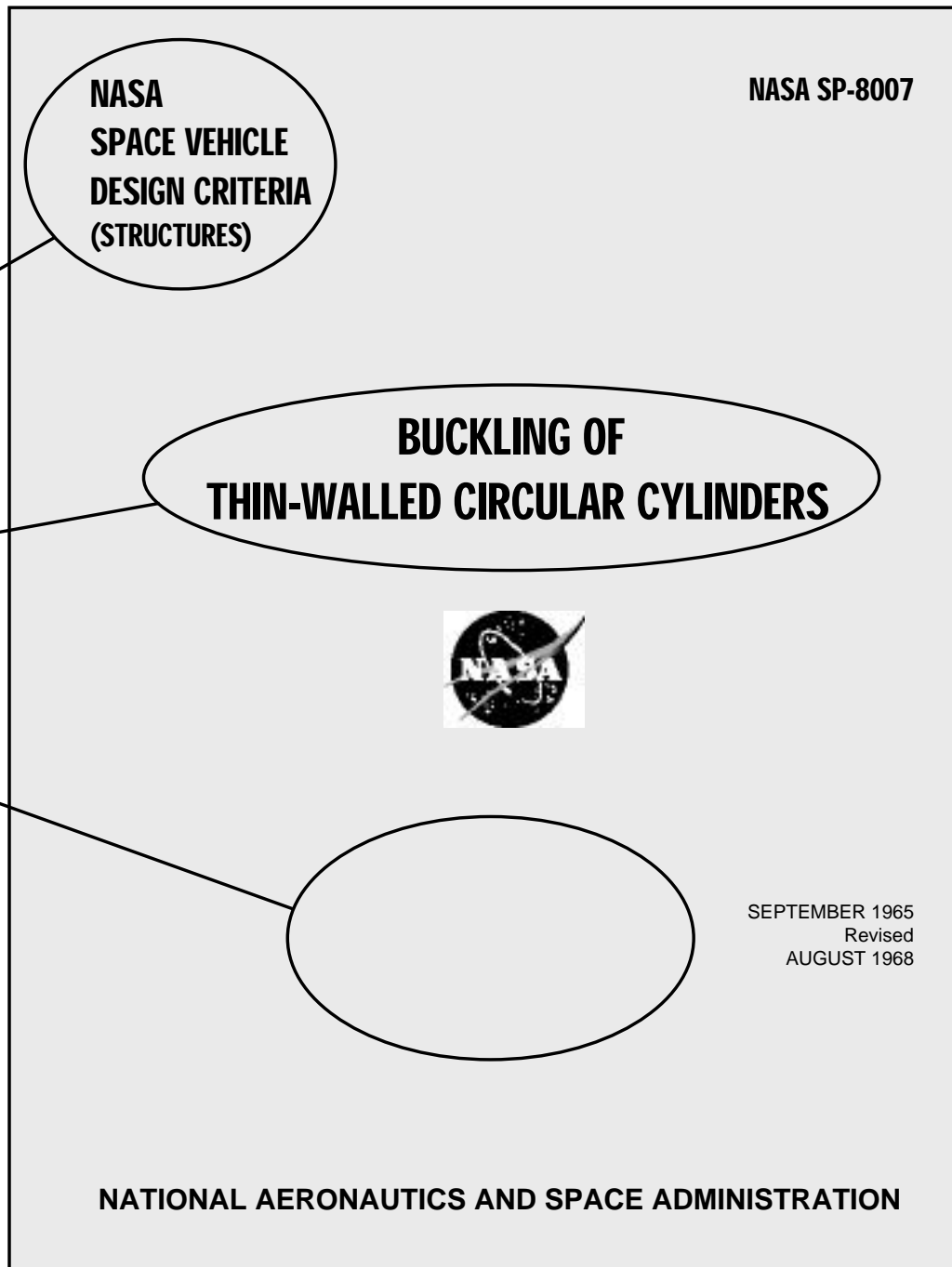
The Classification: “Design Criteria” is a misnomer. “Design Guidelines” is more accurate.

The Scope: One specific response phenomenon. e.g., “Buckling of Thin-Walled Circular Cylinders” instead of “Design of Circular Cylinders”).

Authorship: Broad participation from academia, industry, and NASA. (No single author or editor.)

Theme: What we know. What we think we know. What we think. Supported by equations, data, numbers, AND the caveat that things might change.

References: Extensive. The SP’s basically summarized and applied the current literature.



Suggestion for a New NASA Design Criteria Monograph for Precision Deployment Mechanisms

Scope: Focus on one specific response phenomenon: hysteresis. Why hysteresis? It is the one quantifiable response phenomenon within deployment mechanisms that should be linkable to specific “failure modes” within a deployable structure (e.g., mirolurches, thermal “pops”, etc.)

Theme: *“What we know. What we think we know. What we think.”* Present methods for analyzing and experimentally quantifying hysteretic response. Present design principles and guidelines for reducing hysteresis. Facilitate a merger between optomechanical and aerospace-mechanical design philosophies.

Participation: Representatives from the microdynamics research community and both the optomechanical and deployment-mechanism-design communities. (e.g., NASA LaRC, JPL, CU, Raytheon, AEC Able, SPIE, etc., etc., etc.)

Funding Support: ??????????

NASA SP-XXXX



Hysteresis in High-Precision Deployment Mechanisms for Optical Instrument Structures

National Aeronautics and
Space Administration

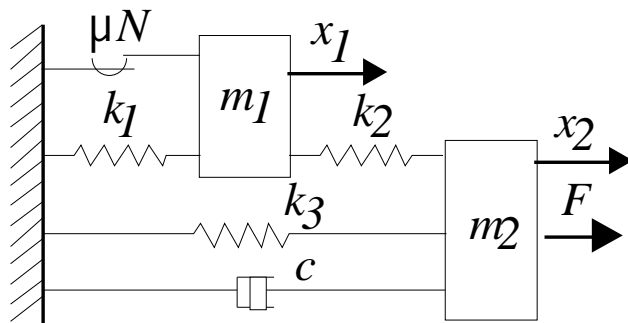
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Suggested Contents of a Precision Deployment Mechanism Design Criteria Monograph

- **Introduction**
 - Linkage between component hysteresis and structural microdynamic failure modes.
- **State of the Art**
 - Deployment mechanism design principles
 - Optomechanical mechanism design principles
- **Criteria**
 - Definition of hysteretic-response criteria
- **Recommended Practices**
 - Analysis methods for facilitating design
 - Test methods for qualifying design

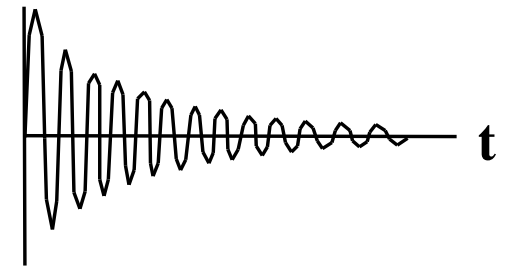
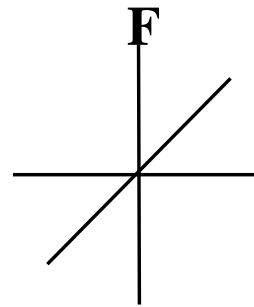
Introduction

Simplified Load-Transfer Model Illustrates Relationship Between Structural Hysteresis and Possible “Mode 1” Microdynamic Failure (Gross Slippage)

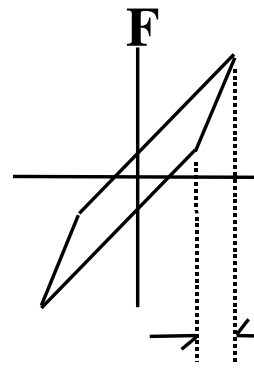


Model Parameters

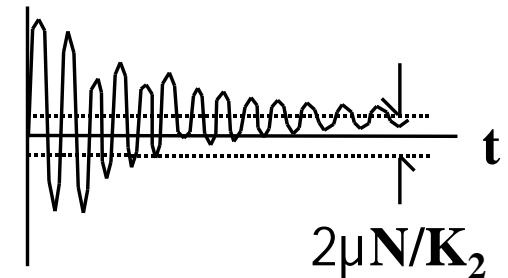
Linear Response Below Stick-Slip Threshold



Nonlinear Response Above Stick-Slip Threshold

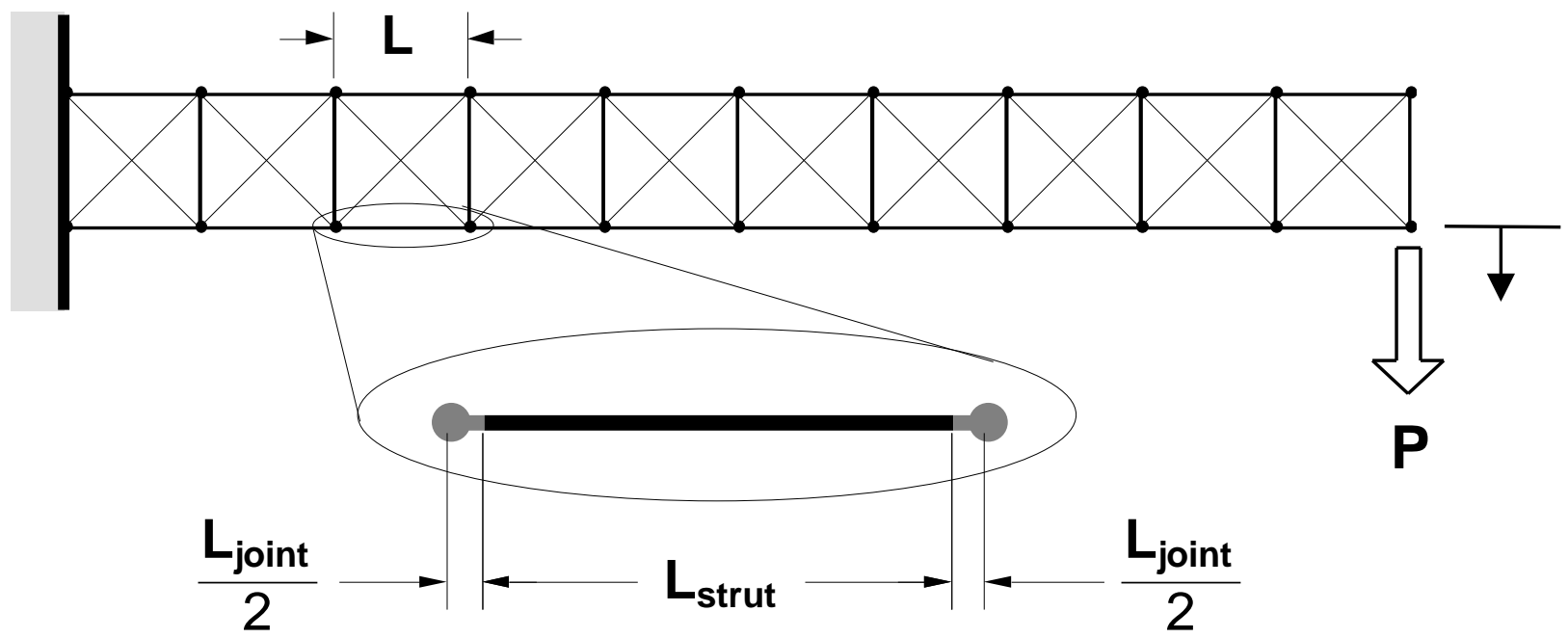


Hysteresis



Microslurch

Mitigating “Mode 1” Failure Involves Minimizing Structural Hysteresis (δ_{total}) By Tailoring Component Stiffness and Hysteresis (δ_{joint})



Linear response:

$$= \frac{P(nL)^3}{3(EI)_{eff}} = \frac{Pn^3}{3} \left(\frac{L_{joint}}{(EA)_{joint}} + \frac{L_{strut}}{(EA)_{strut}} \right)$$

Total (linear + hysteretic) response:

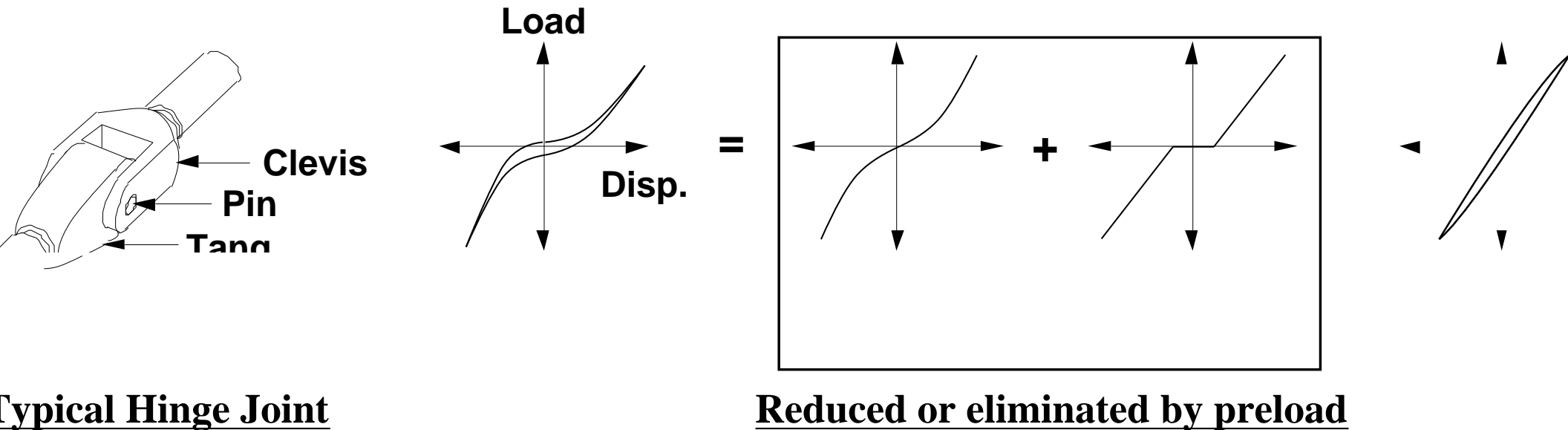
For any determinant truss with identical struts and joints, structural hysteresis is minimized when $\delta_{joint} = \delta_{strut}$

$\delta_{total} = \delta_{joint} + \delta_{strut}$

State of The Art

State of the Art in Deployment Mechanism Design

- The true state of the art in high-precision deployment mechanisms is difficult to establish due to the possible classified experience.
- The unclassified literature indicates that the majority of applications are sub-optical-precision (i.e., solar arrays and RF antennas).
 - Hachkowski, M. R., and Peterson, L. D., A Comparative History of the Precision of Deployable Spacecraft Structures, University of Colorado publication CU-CAS-95-22, December, 1995.
- Emphasis tends to be on simplicity (i.e., low part count), low mass, high stiffness. Nonlinearities reduced PRIMARILY through preload.



State of the Art in Optomechanical Design

- **Numerous publications present design principles for optical-precision mechanisms such as positioning devices and kinematic mounts.**
 - Jacobs, D. H., Fundamentals of Optical Engineering, McGraw-Hill Book Co., 1943.
 - Vukobratovich, Daniel, "Principles of Optomechanical Design," in Applied Optics and Optical Engineering, Vol. 11, R. R. Shannon and J. C. Wyant, ed, Academic Press, 1992.
- **These principles are presented implicitly, through the discussion of specific examples. (Therefore, it is not obvious how these principles might be applied to the design of deployment mechanisms.)**
- **Emphasis tends to be on the use of deterministic geometries (e.g., kinematic mounts) and non-conforming interfaces (e.g., spherical contacts) as opposed to stiffness/strength concerns.**



Figure from Vukobratovich's reference depicting "optically quiet"
1-, 2-, and 3-DOF constraints

Criteria

A Useful Criterion on Deployment Mechanism Performance is One Derived from a Specific Microdynamic Failure Mode and Relatable to Specific Design Principles. . .

$$\text{total} = \frac{\text{Recommended practices derived from optomechanical design principles}}{1 + \left(\frac{\left(\frac{EA}{L} \right)_{\text{joint}}}{\left(\frac{EA}{L} \right)_{\text{strut}}} \right)} \text{Maximize joint stiffness}$$

Recommended practices derived from deployment mechanism design principles

Recommended Practices

*Just “spice up” our existing deployment mechanism design practices
with a “dash “of optomechanical design principles. . .*

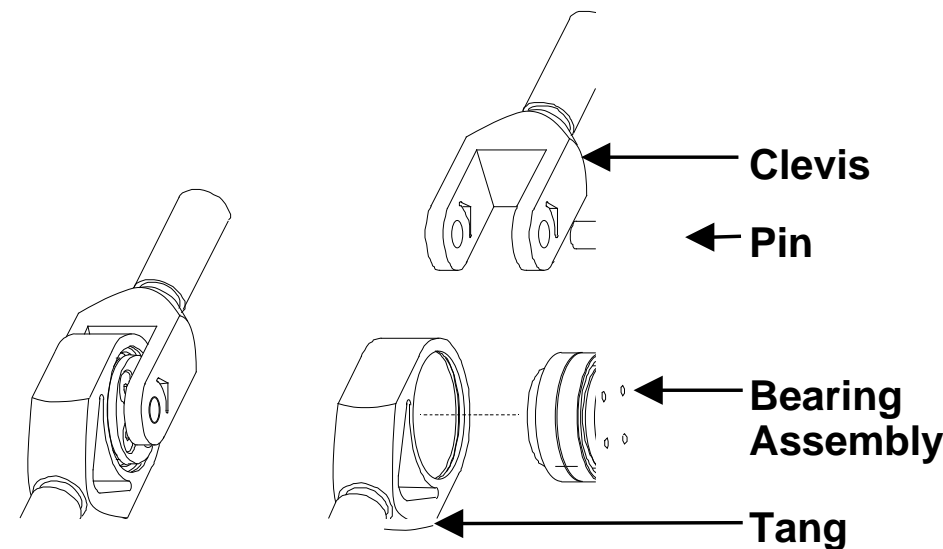
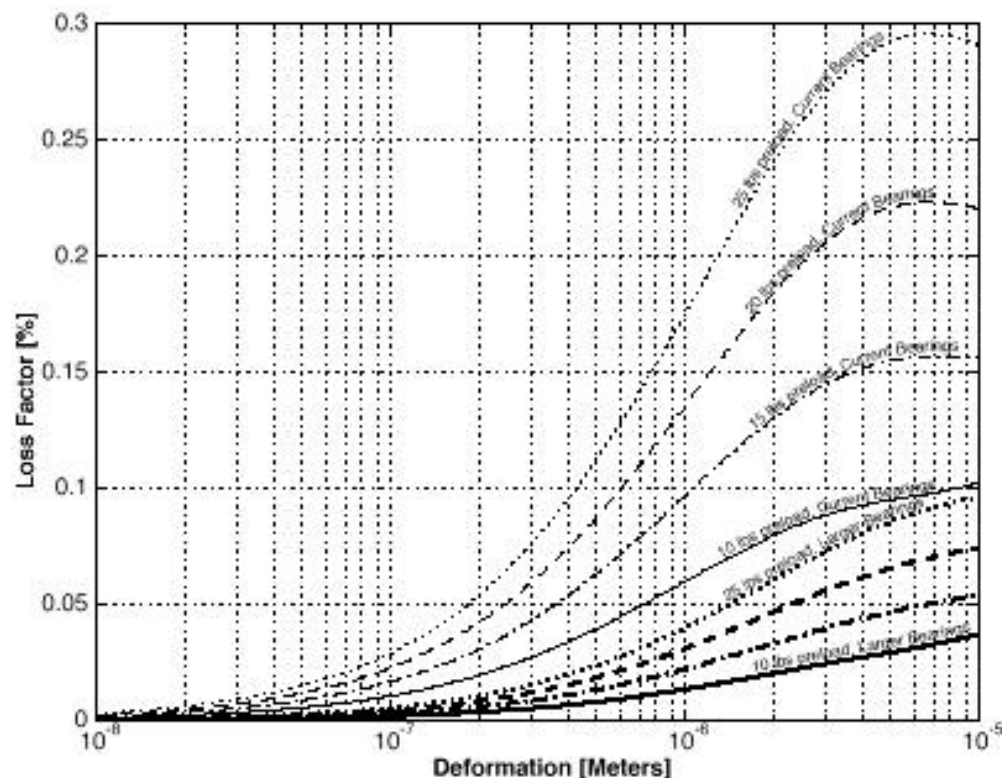
In a Sense, Dr. Hachkowski Performed Detailed Hysteretic-Response Analyses of Deployment Mechanisms, and out “fell” the Optomechanical Design Principles!

- Hachkowski, M. Roman: “Reduction of Hysteresis in the Load-Displacement Response of Precision Deployment Mechanisms Through Load Path Management,” University of Colorado, 1998
- **Objectives:**
 - Establish precedents for modeling interface contact mechanics and their effects on stiffness and hysteresis in precision deployment mechanisms.
 - Derive design principles for minimizing hysteresis and maximizing stiffness in precision deployment mechanisms.
- **Principal Contributions:**
 - New theoretical model of rolling element mechanics including interface stiffness and nonlinear friction microslip.
 - “Load-Path Management” design methodology, which is relatable to optomechanical design principles.



Hachkowski's Detailed Modeling of Contact Mechanics Within a Precision Hinge Led to Substantial Design Insight

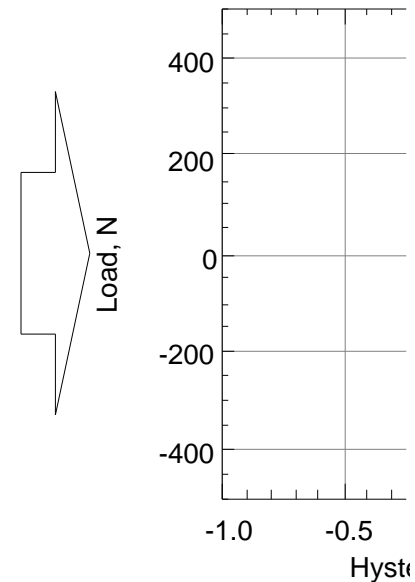
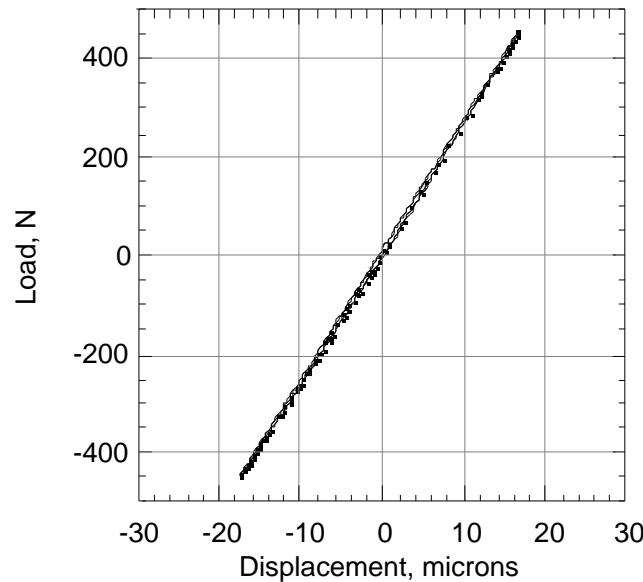
- In general, hysteretic “loss factor” varies with response amplitude:
 - collapsing to material loss factor at low amplitude (Mode 3/4 failure regime?)
 - reaching a peak at a moderate amplitude (Mode 1/2 failure regime?)
- For this specific joint design:
 - larger bearings DECREASE loss factor.
 - larger preloads INCREASE loss factor.



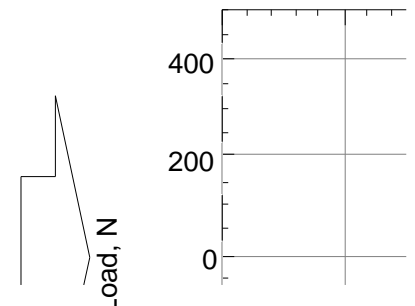
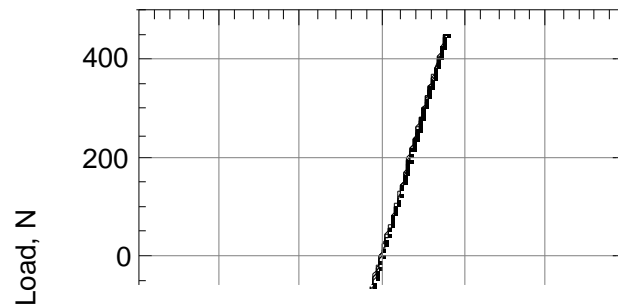
Composite Version of Hinge Joint Developed to Exhibit Higher Stiffness (and Lower CTE) Than Prototype Aluminum Hinge

- Same internal (i.e., bearing and press-fit pin) design
- Thicker, higher-modulus composite tang and clevis

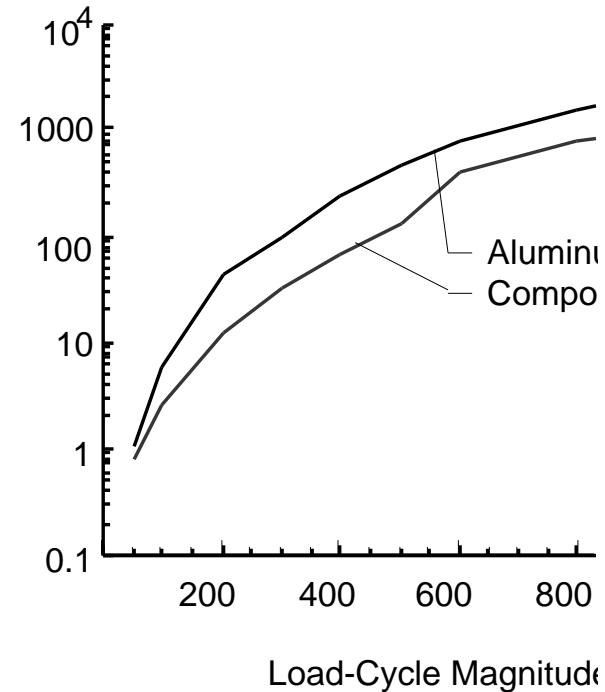
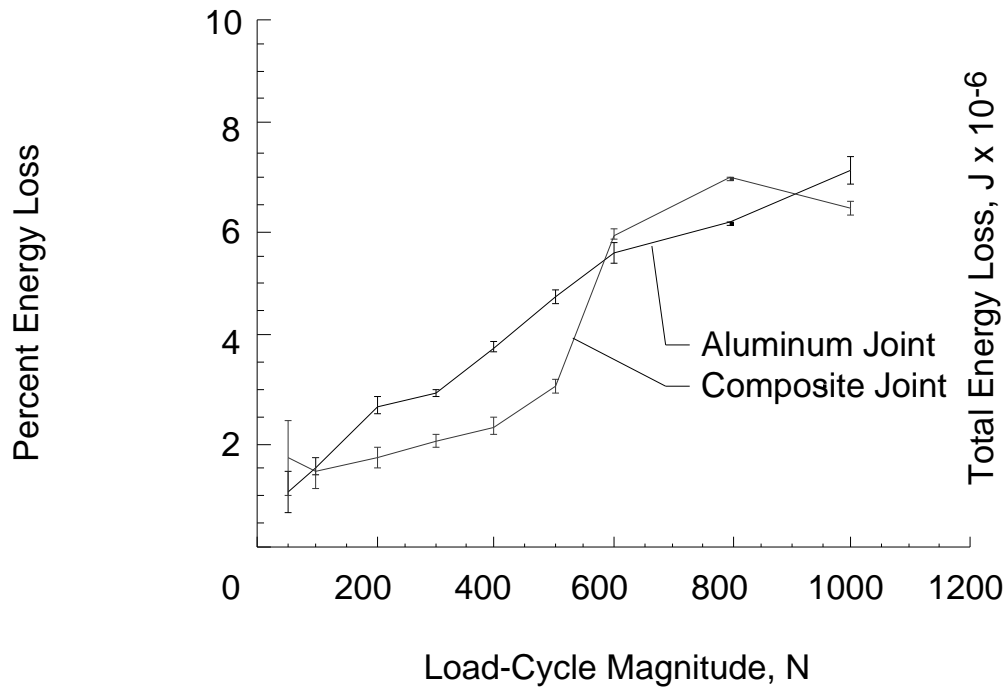
Aluminum Hinge Data
(Gage Length = 3.5")



Composite Hinge Data
(Gage Length = 2.75")



Results Indicate that Their Can be a Synergistic Effect on Hysteresis of Increasing the Joint Stiffness



Higher loss factors in the aluminum joint are likely due to local elastic deformation of the pin and slippage of the pin interfaces.

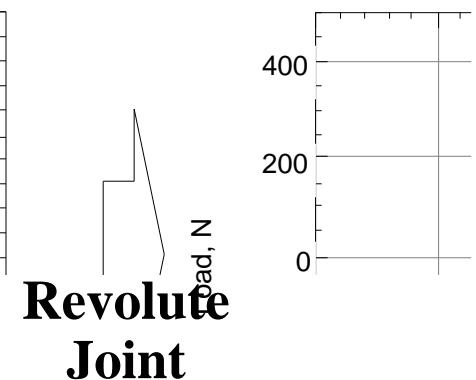
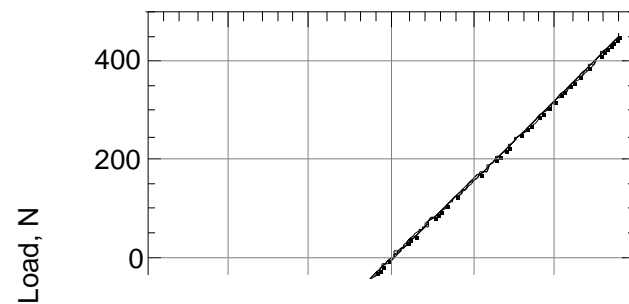
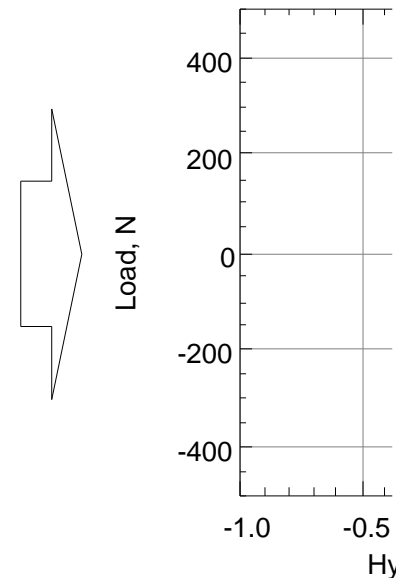
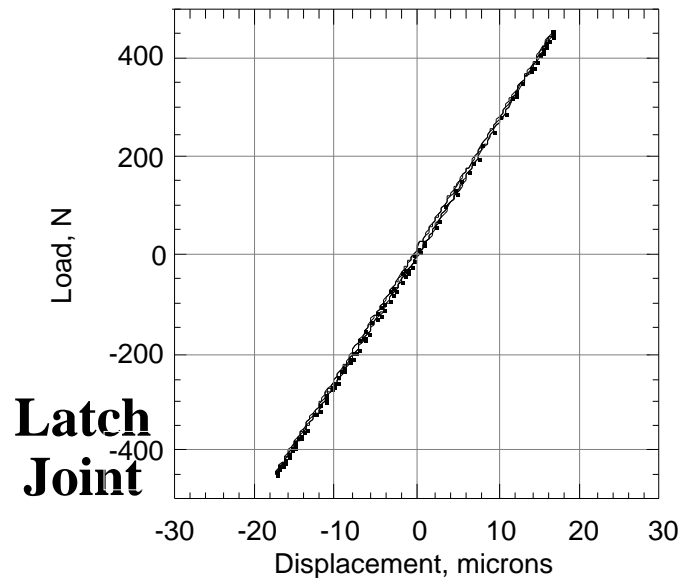
Similar Results From a Precision Latch Indicate that Achieving Extremely Low Hysteresis Might Require Sacrifice to Stiffness

- Larger-diameter bearing than the prototype hinge
- Larger-diameter press-fit assembly pin than the prototype hinge

Hinge Joint Data
(Gage Length = 3.5")



Latch Joint Data
(Gage Length = 3.8")



Summary

Adequacy of any engineering design can only be defined relative to some accepted standards or criteria.

Until we develop such criteria for precision deployment mechanisms, the issue of microdynamics will remain controversial and difficult for missions to deal with.